



One
GREAT
Team

Southern Company Generation

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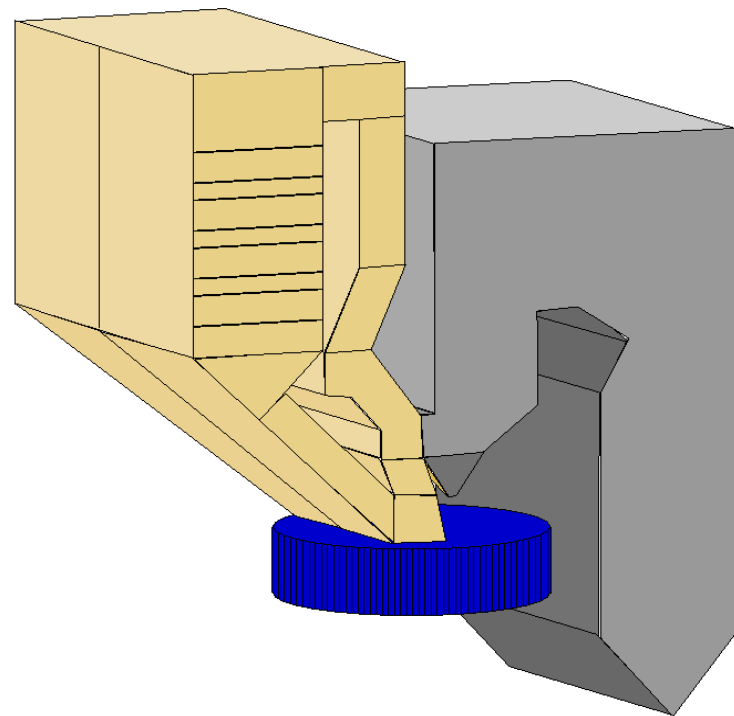
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SCR Flow Modeling

- Basic Introduction
- Case Studies
 - Scherer 3 & 4 (Physical Model, design phase)
 - Miller 3 (CFD, to address maintenance concerns)

Why is Flow Distribution Important to SCRs?

- Performance
 - Gas velocity uniformity
 - Uniform NH_3 -to- NO_x ratio
 - Thermal mixing
 - Ash capture / build-up
- Operating costs
 - Pressure drop
 - Erosion
 - Corrosion



Fluid Dynamic Design Methods

- Physical Flow Modeling
 - Lab representation of geometry
 - Typical scale 1:8 to 1:16
 - “Cold flow” modeling
 - Visualize flow with smoke
 - Simulate ash deposition
 - Measure flow properties:
 - velocity, pressure, tracer gas



Typical 1/12 scale physical model

- Turning vanes

- AIG w/static
mixers

- Economizer
bypass

- Economizer
outlet

- LPA screen

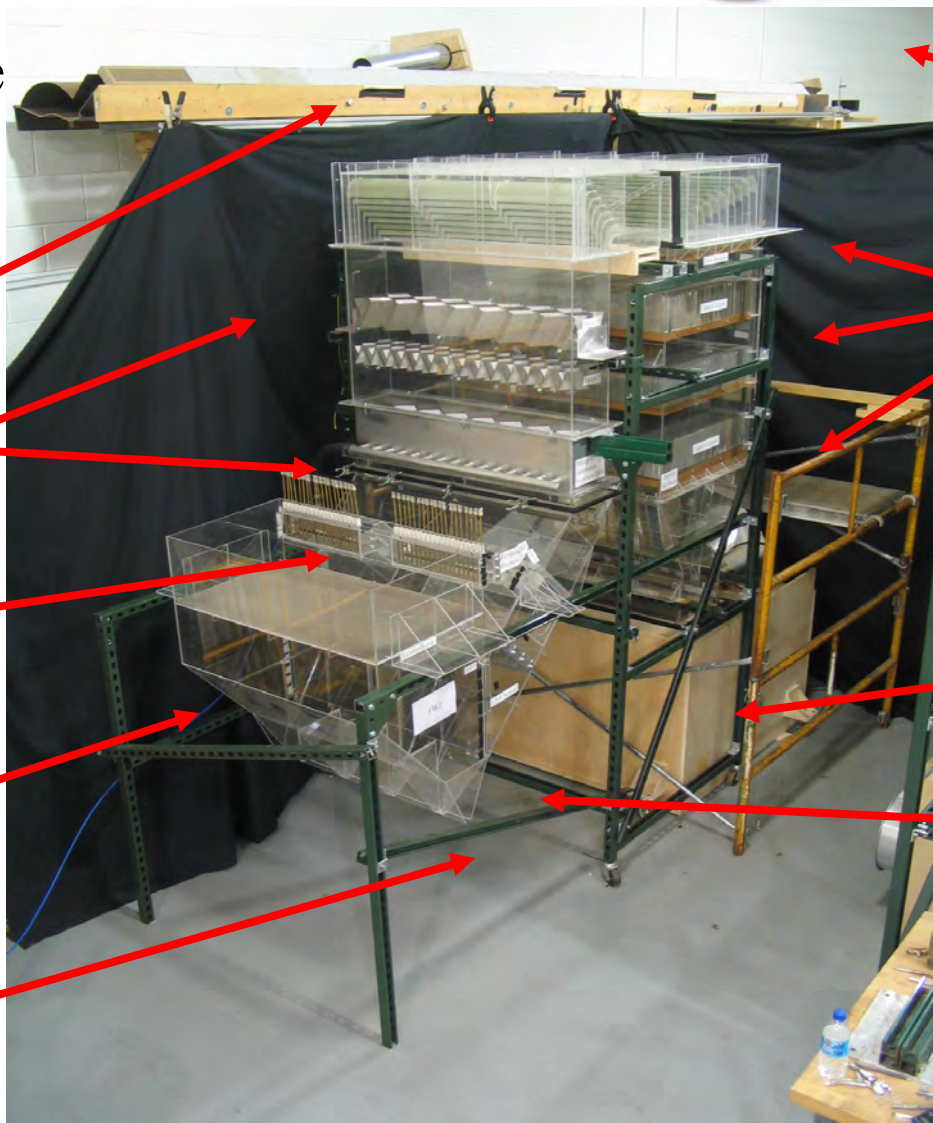
- Vanes

- Rectifier

- Catalyst layers

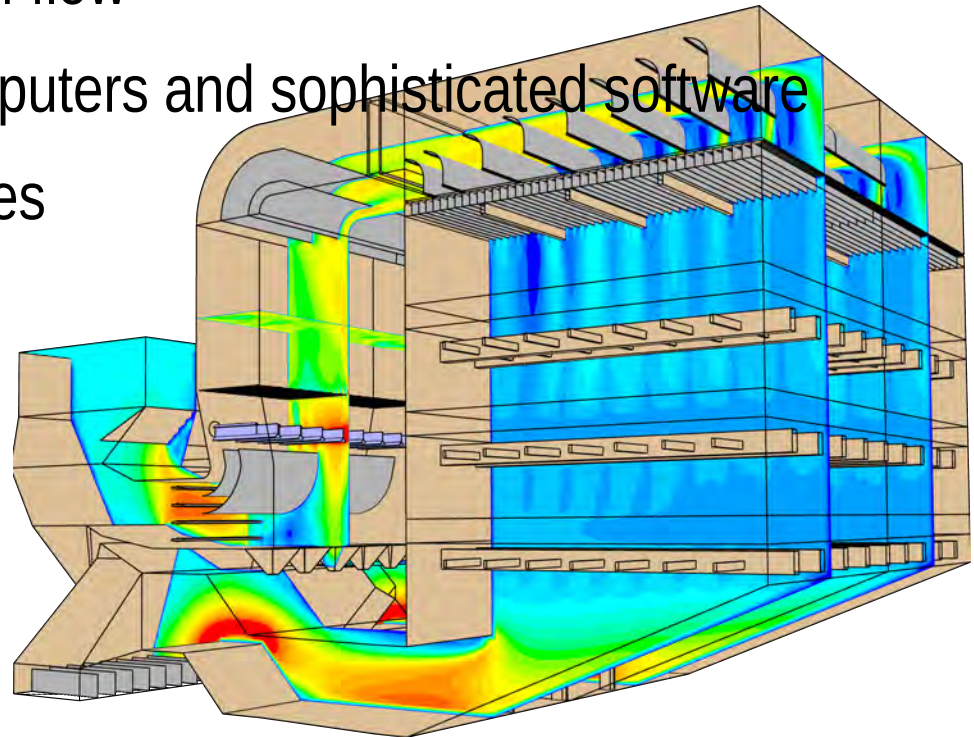
- Air heater

- Dampers



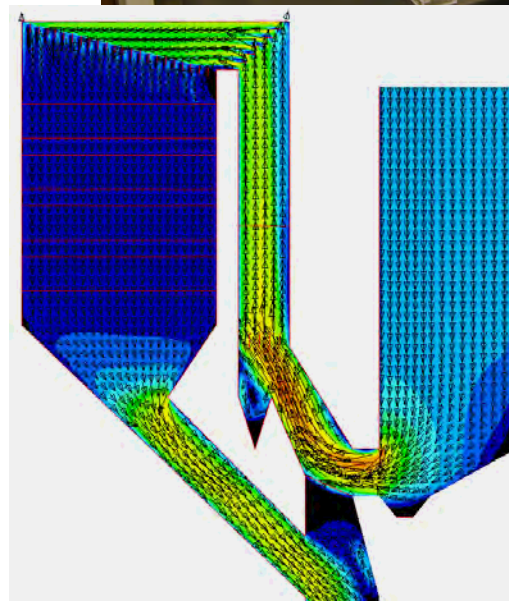
Fluid Dynamic Design Methods

- Computational Fluid Dynamics (CFD)
 - Numerical simulation of flow
 - Utilize high speed computers and sophisticated software
 - Calculate flow properties
 - Velocity & Pressure
 - Temperature
 - Ammonia
 - Particle streamlines



SCR Performance Goals

- Uniform velocity
- Uniform temperature
- Uniform NH_3 -to- NO_x ratio
- Avoid ash build up, LPA carryover
- Minimize DP



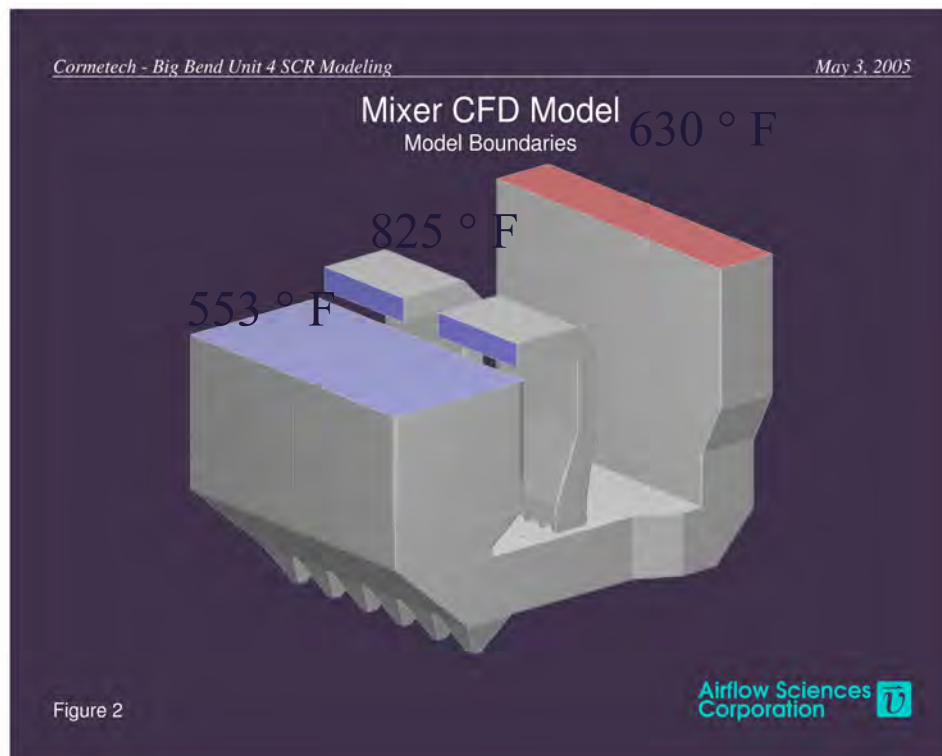
SCR Velocity Distribution

- Velocity profile
 - At AIG
 - At SCR inlet
 - At AH inlet
- Directionality
 - At SCR inlet



SCR Thermal Mixing

- Economizer gas bypass used to boost SCR inlet gas temperature under low load operation
- Extract hot gas at econ inlet
- Inject into cooler econ outlet stream
- Sounds simple enough, but there are many options and competing design elements

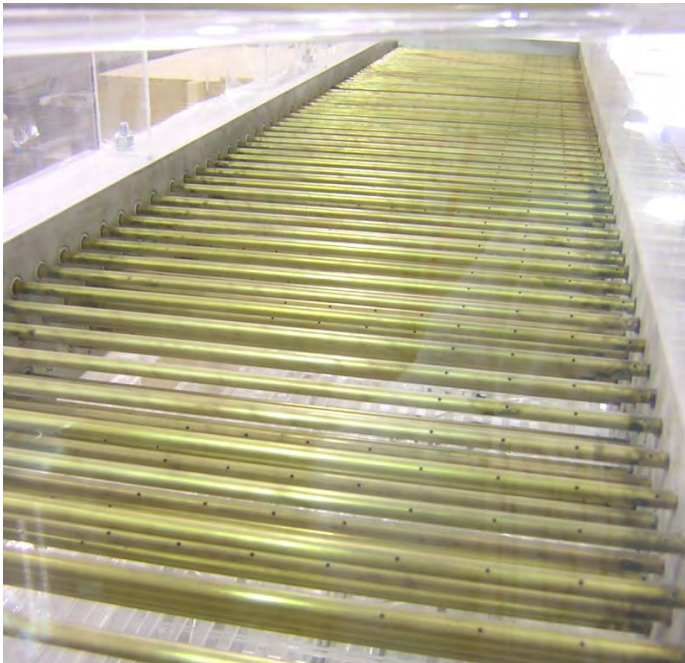


Without mixer, $\Delta T = \pm 83\text{ }^{\circ}\text{F}$

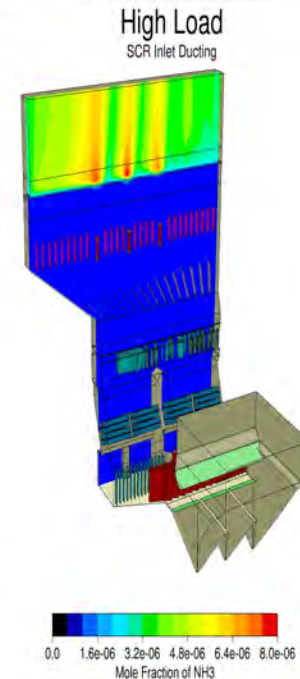
With mixer, $\Delta T = \pm 15\text{ }^{\circ}\text{F}$

SCR Ammonia Injection

- Tracer gas in physical model
- Species tracking in CFD



Corneltech - Roxboro Unit 2 Backpass and SCR Modeling

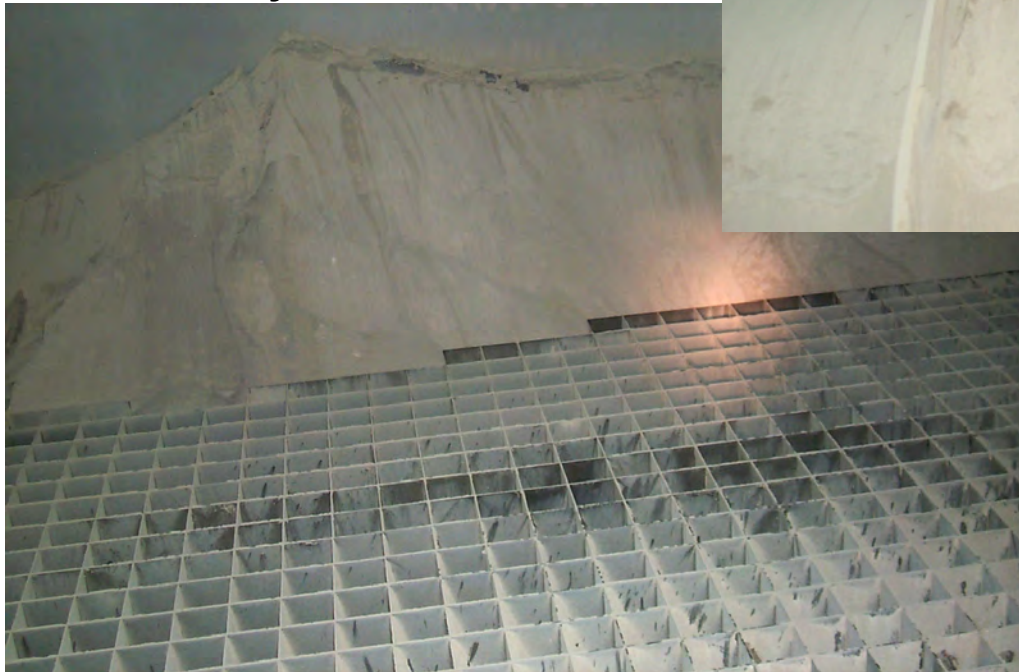


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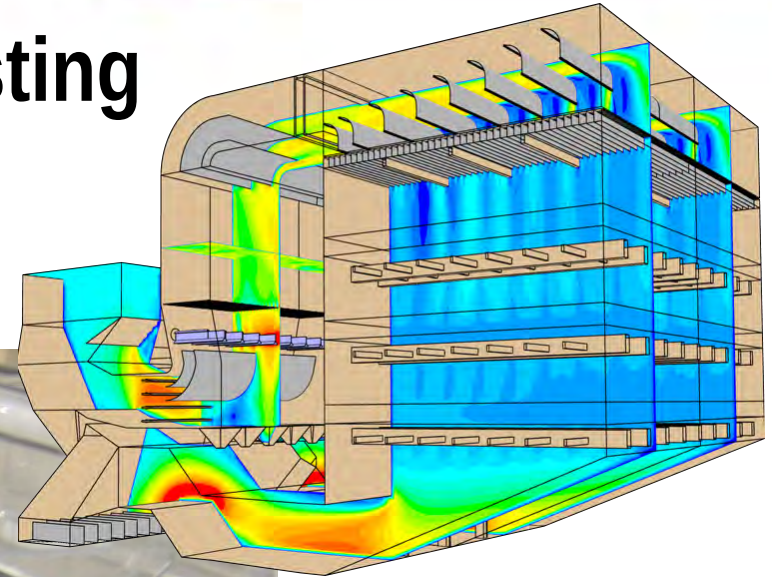
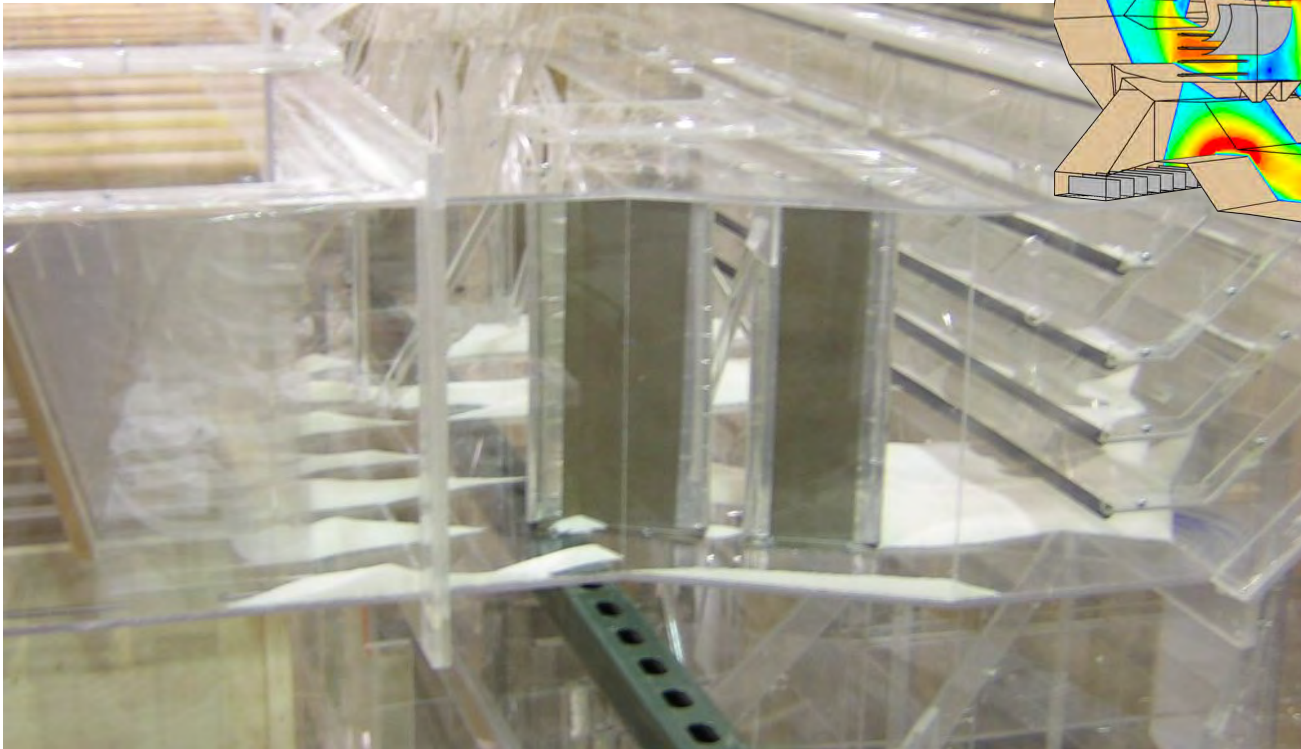
Ash Deposition

- Duct floors
- Turning vanes
- Catalyst



Ash Deposition – Model Testing

- Drop out
- Re-entrainment



Model Accuracy

- Data for detailed correlation between models and actual plant operations is unfortunately limited
 - Detailed traverses at catalyst often not performed
 - Data in ductwork sometimes available
 - Tend to go by industry experience on whether catalyst performance goals are met
- In cases where CFD and physical models are both used, predictions are often within engineering tolerances (~10-20%), but not always
- Further analysis is needed and in progress

Points to Remember

- Gas flow patterns have significant impact on the performance of SCRs
- Analysis and design tools include physical and CFD flow modeling
- Models are used to optimize the design of flow control devices to achieve fluid dynamic goals
 - Ductwork, turning vanes, baffles
 - Mixers, injection systems
 - LPA mitigation baffles, screens, and hoppers

2 Case Studies

- Scherer 3 & 4 Physical model
- Plant Miller CFD models

Case 1 Scherer Units 3 & 4 SCR Modeling

- New SCRs on existing Units



Project Overview

- Objective
 - Develop design of flow devices to optimize SCR performance
- Methods
 - Modeling for flow device design and NH₃ mixing verification
- Domain
 - Start at Economizer
 - End at Air Heater Inlet
- Flow conditions
 - Peak, Full, Minimum and Bypass Mode

Modeling Goals

- Flow uniformity
 - Velocity downstream of AIG:
80% of pts within 10% (Target) or 15% (Min) of avg, 100% of pts within 15% of avg
 - Velocity upstream of LPA Screen:
100% of pts within 15% of avg
 - Velocity at reactor inlet:
90% of pts within 10% (Target) or 15% (Min) of avg
100% of pts within 15% (Target) or 20% (Min) of avg
 - Velocity at Air Heater:
100% of pts within 25%(Target) or 35% (Minimum) of avg
 - NH₃ Distribution at reactor inlet:
<3% RMS (Target), <5% (Minimum)
- Minimize pressure drop
- Avoid ash accumulation

Model Results Overview

Peak Load

<u>Parameter</u>	<u>Target Goal</u>	<u>Model Result -Peak</u>
Velocity Downstream AIG	80% of pts within 10% of average	97.9%
Velocity Downstream AIG	100% of points within 15% of average	100%
Velocity Upstream LPA Screen	100% of points within 15% of average * goals changed during project	54.3%
Velocity Upstream first catalyst	90% of points within 10% of average	96.3%
Velocity Upstream first catalyst	100% of pts within 15% of average	97.5%
NH3 Distribution	RMS <3%	2.6% RMS
Velocity at Air Heater Inlet	100% of points within 25% of average min goal 100% of pts within 35% of avg	87.5% 100%
Total pressure drop, economizer outlet to air heater inlet	Excluding catalyst pressure loss	3.89"H2O

Physical Model

- Methodology
 - 1/12 scale model represents geometry
 - Scaled flow rates to match velocity head between model and full scale
 - Incorporates important structure (vanes, trusses)
 - Catalyst modeled as honeycomb and perforated plates
- Measurement techniques
 - Velocities using vane anemometer, hot wire
 - Pressures using pitot probe
 - Ammonia injection simulated with tracer gas
 - Ash drop-out and re-entrainment simulated with salt

Physical Model Results Summary

Test Plane

Ash Testing

- Purpose
 - Determine areas where ash will drop out at reduced loads
 - Examine if ash is properly re-entrained when higher load is restored
- Assumptions
 - Model dust behaves similarly to ash
 - » Utilize wind tunnel data to compare model dust to actual ash
 - » Run model at correct velocity ratio to provide best comparison
 - Ash is not wet, cindered/hardened, packed solid in a cavity, etc.

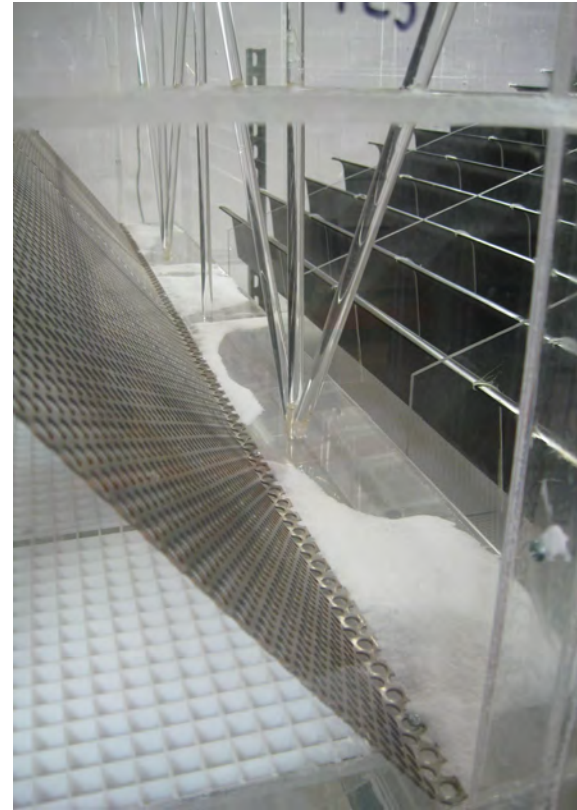
Ash Deposition Testing Process

- Low load velocity setting
- Dust injected at economizer and downstream of AIG
- Dust injected until a stable depth was achieved

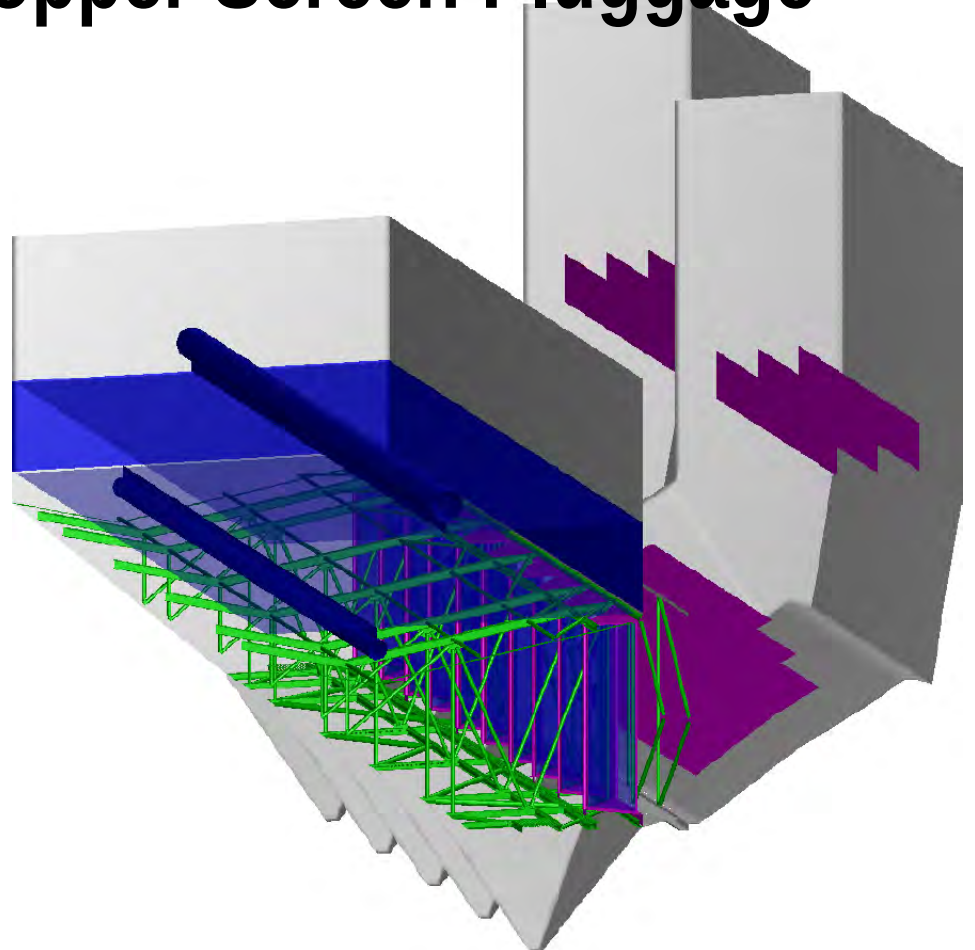


Ash Re-Entrainment Testing Process

- Dust was deposited on horizontal surfaces to approximately 0.5-1" depth
- Flow was slowly increased to full load velocity
- Ash re-entrainment was observed and documented



Case 2: Miller Econ Hopper Screen Pluggage

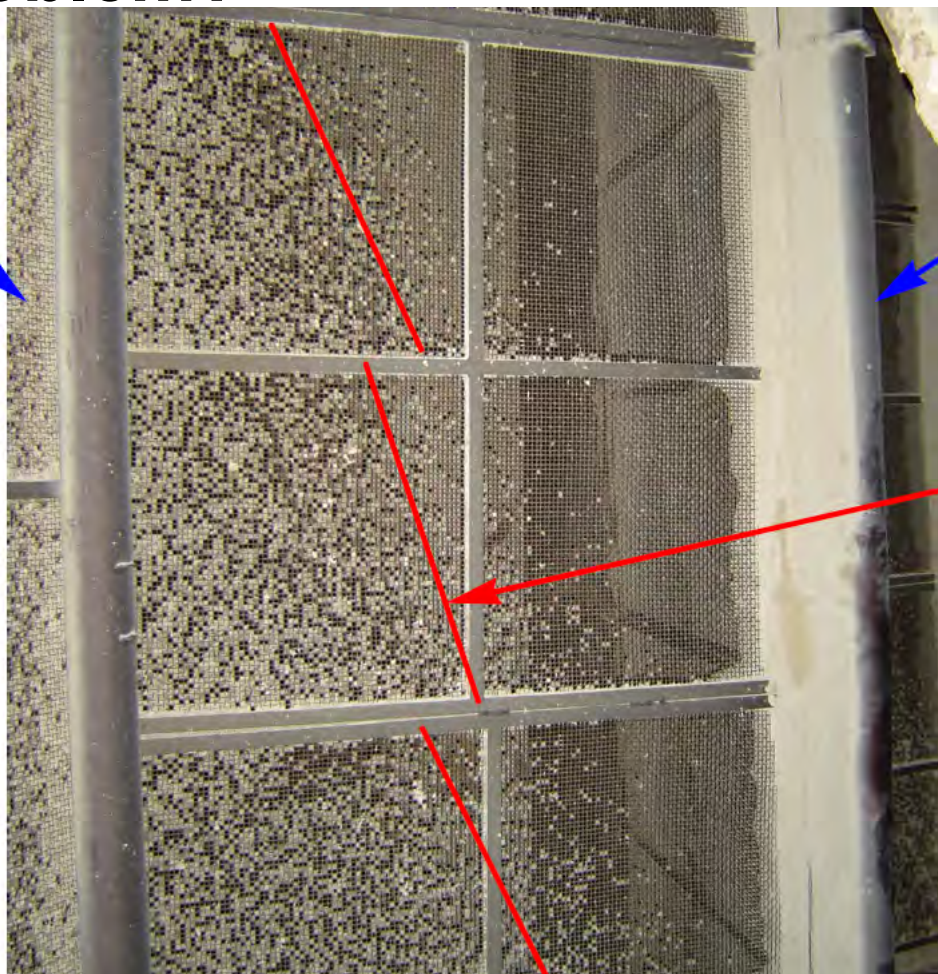


What's the Problem?

- Pleated Screen

Valley

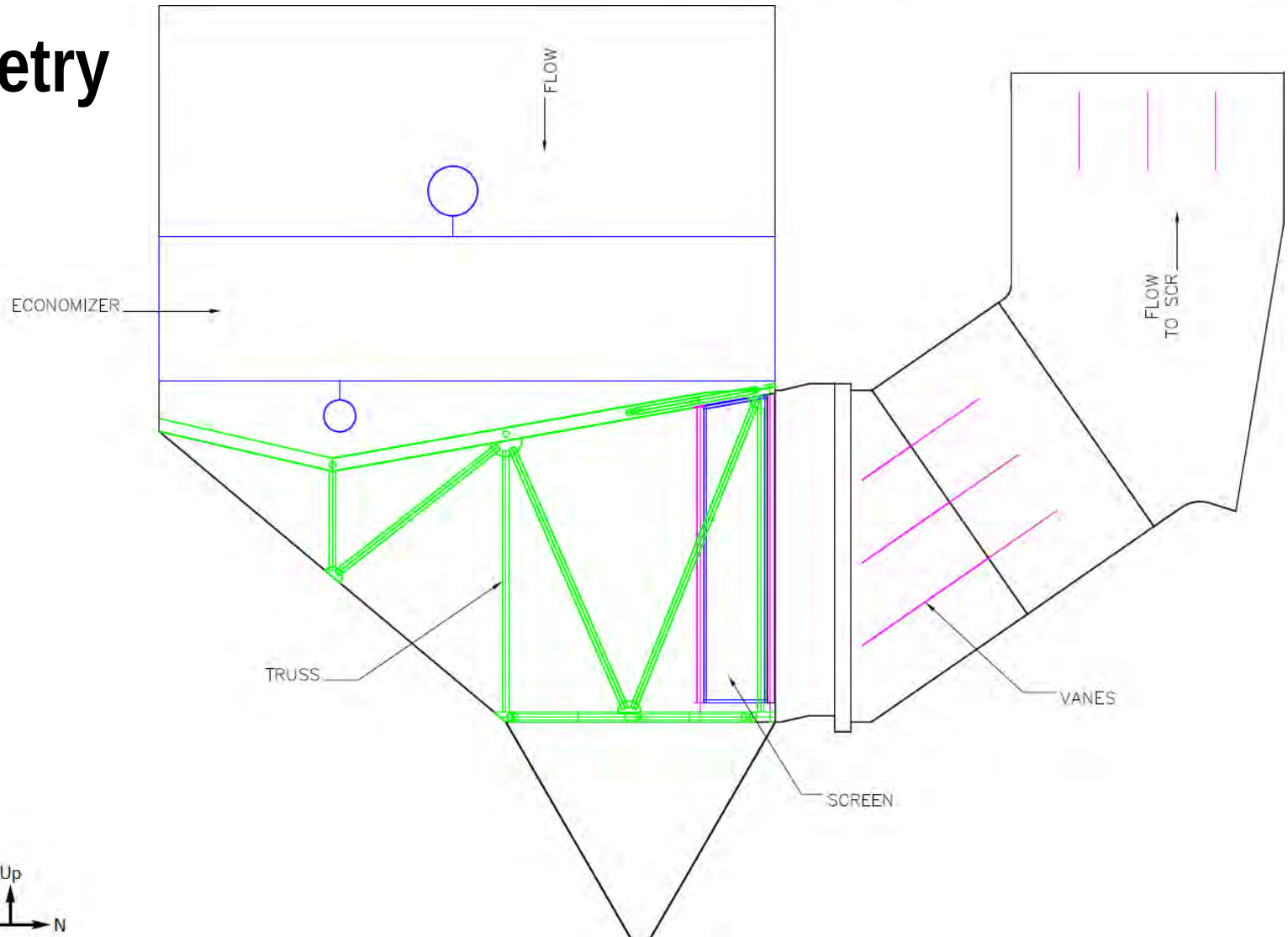
- DP slowly increases as the unit runs
- Why? LPA screen becomes plugged



Peak

Approximate
Edge
of Pluggage

Geometry



Pleated Screen Details Must Be Included



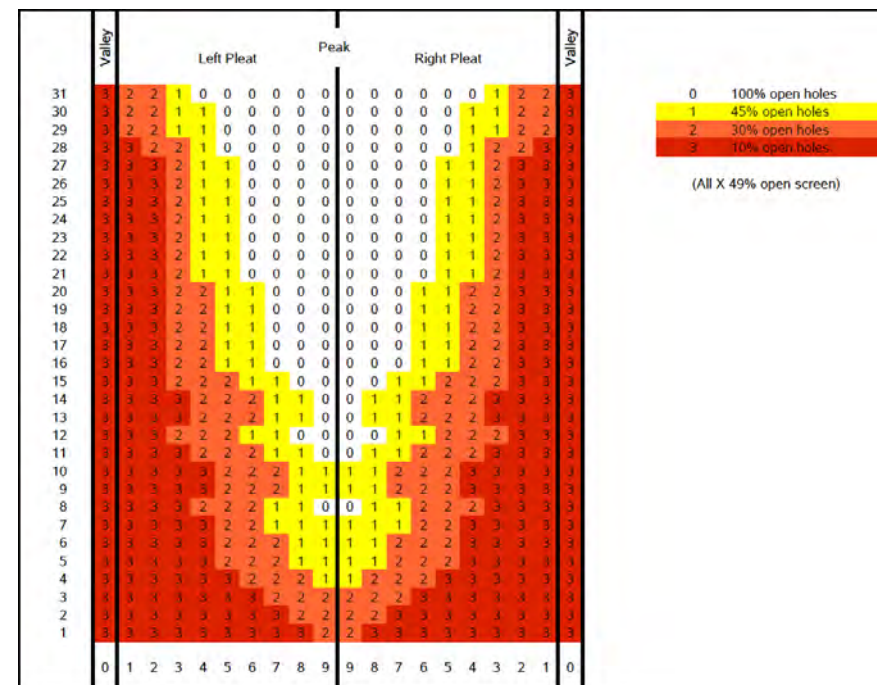
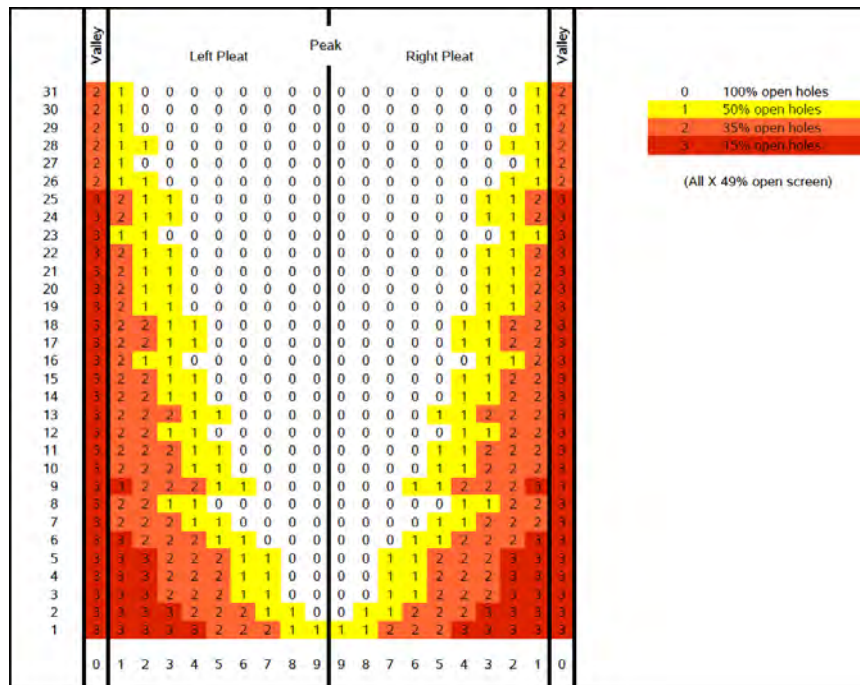
Particle Characterization

- Plugging particles measured
- Drag and rebound characteristics of LPA



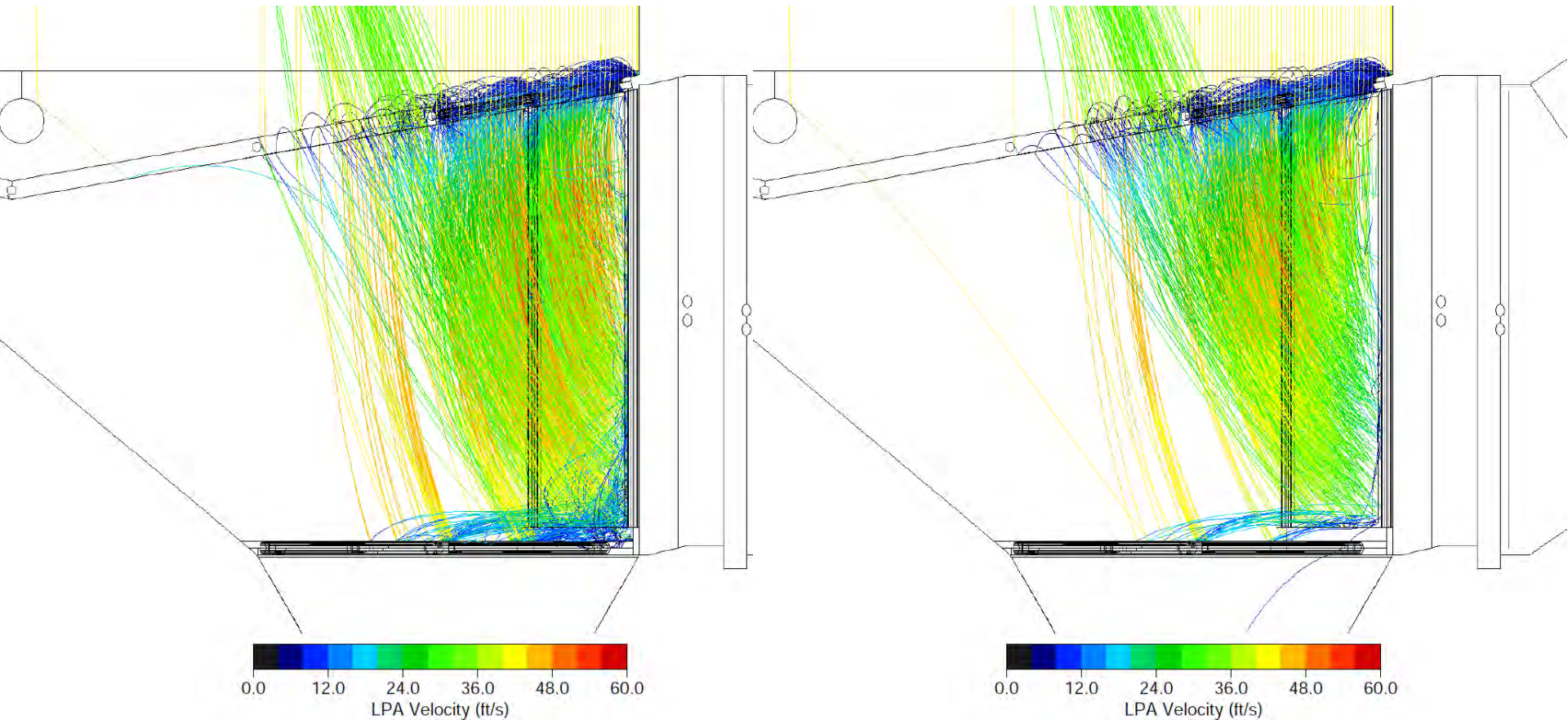
How to model changes due to buildup?

- 3 conditions modeled:
 - Clean, partially plugged, strongly plugged



5mm Particles Striking the Screen

- Clean on right, strongly plugged on left

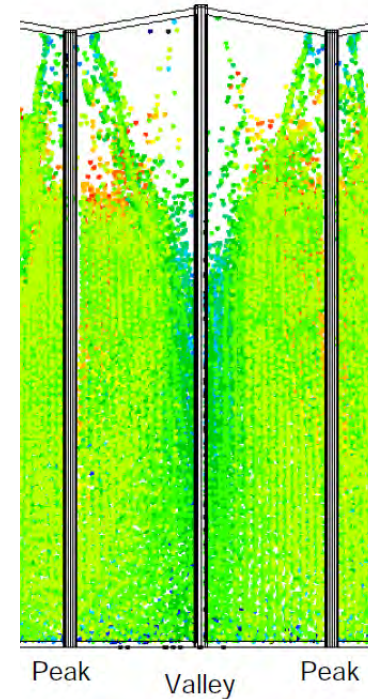
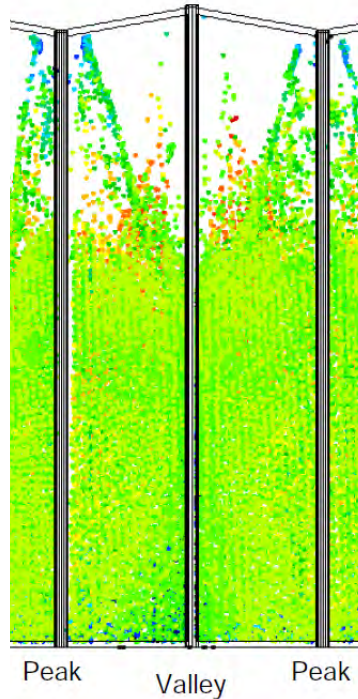
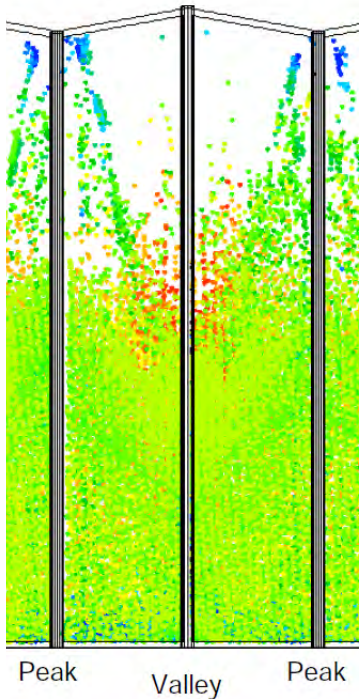


Some Shift in Pluggage Pattern over Time

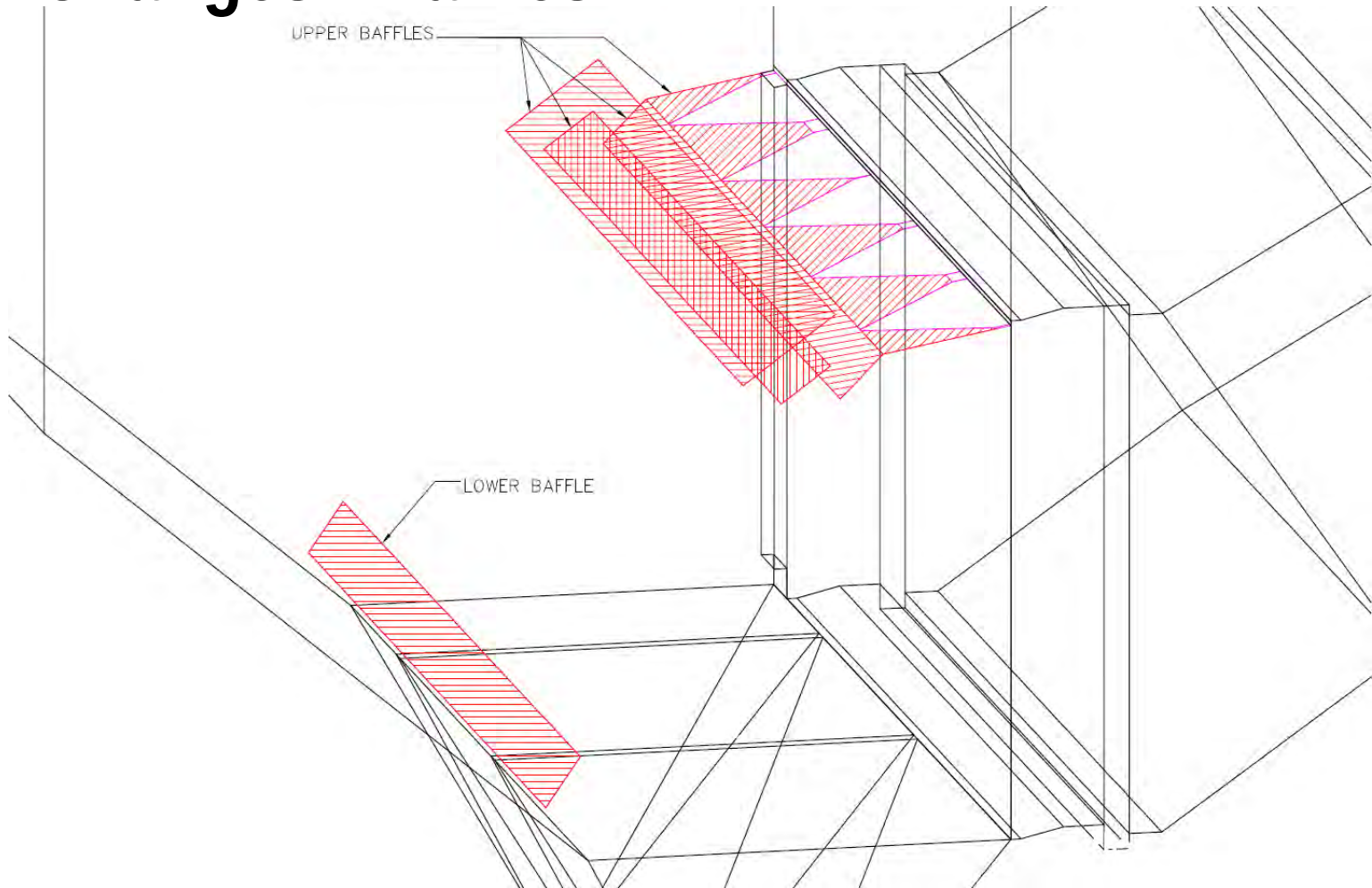
- Clean

Partial Plugged

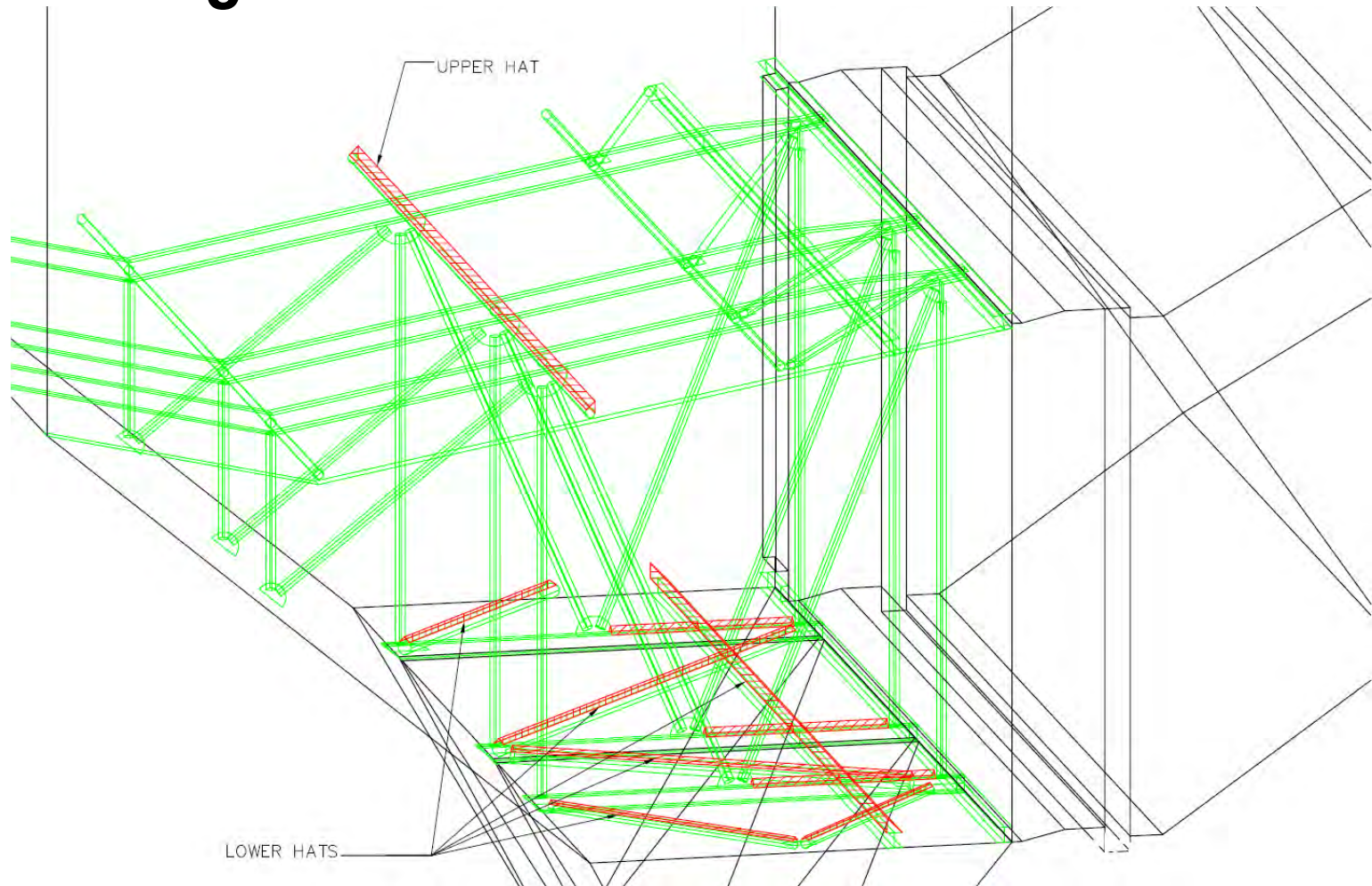
Strongly Plugged



Design Changes - Baffles

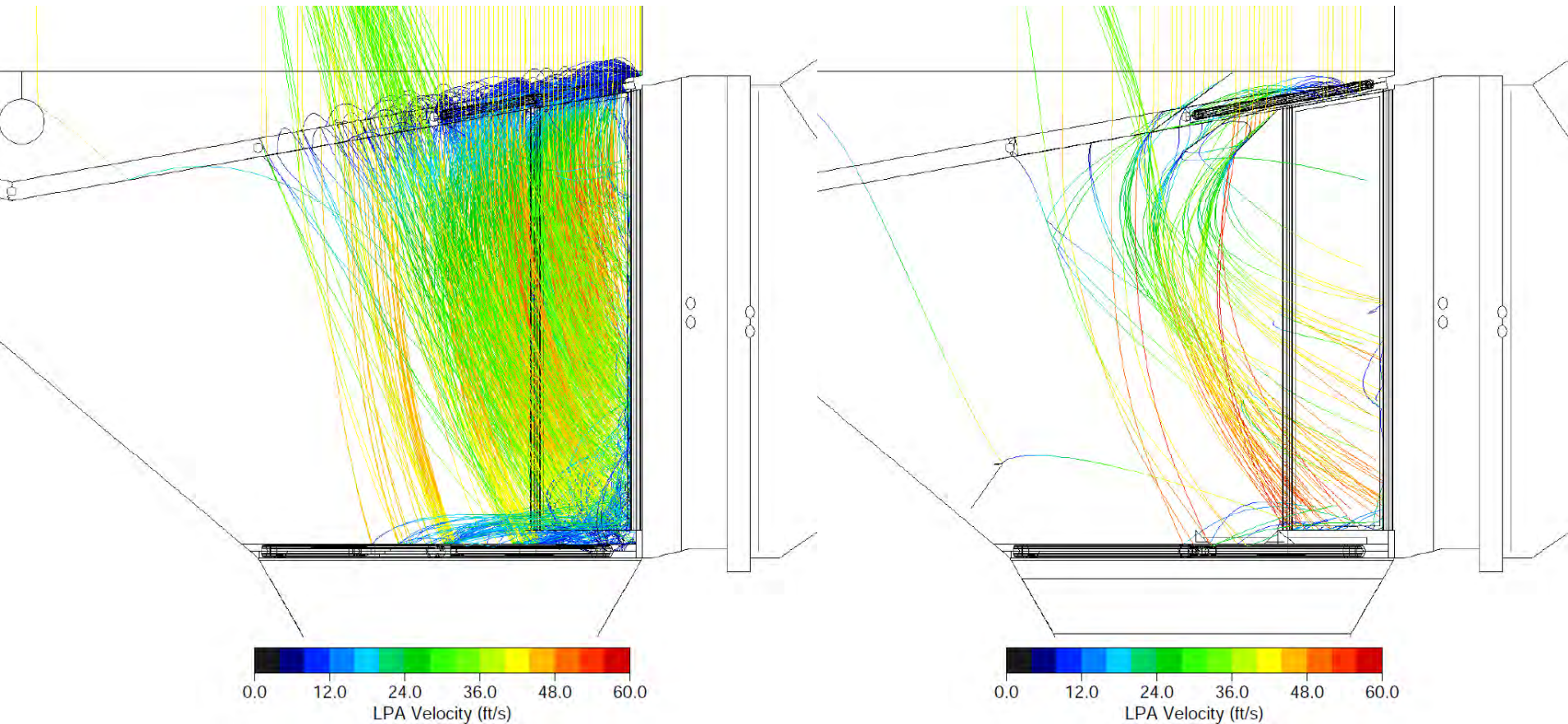


Design Changes – “Hats”

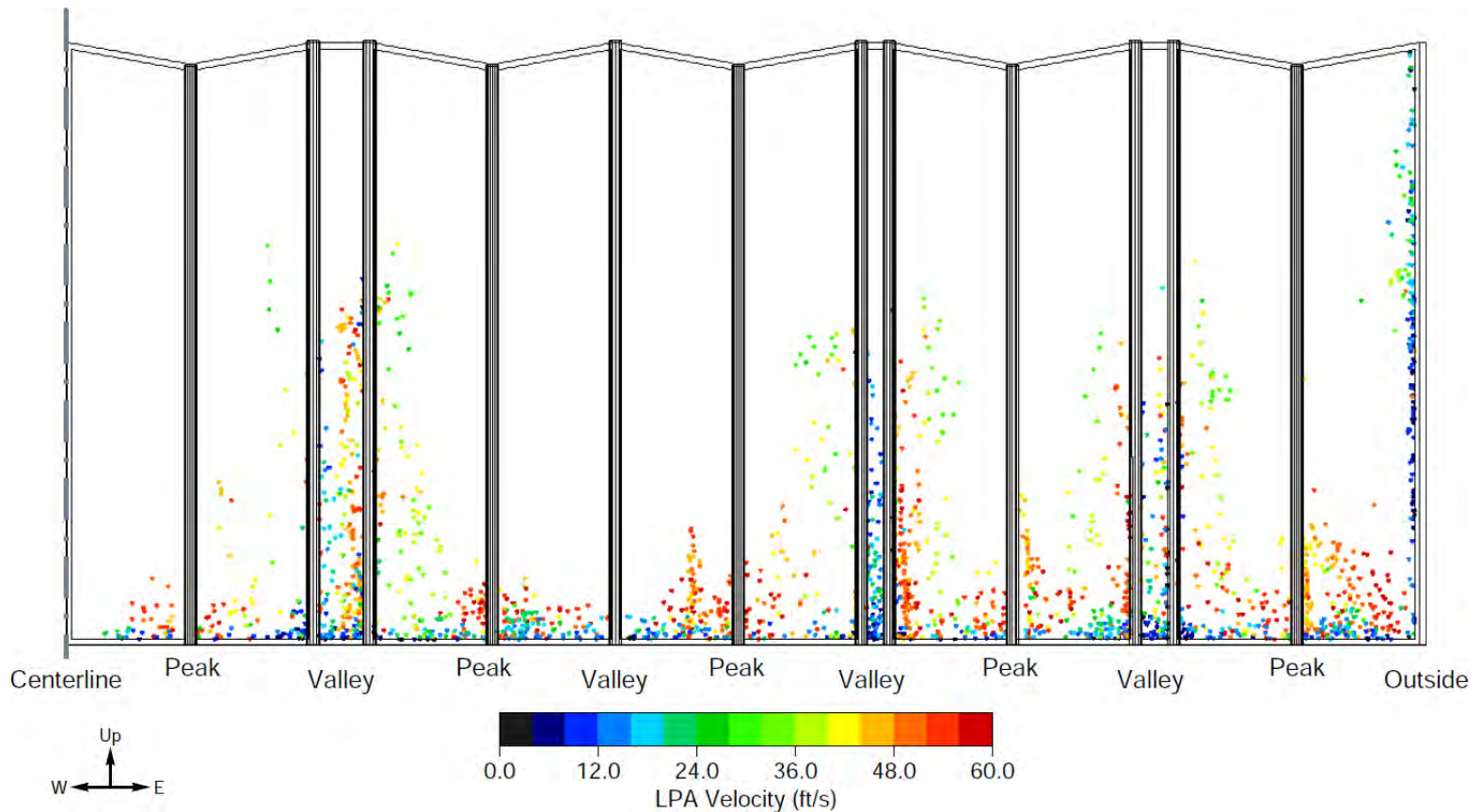


Drastically Reduced Impacts

- Baseline on left, final design on right



Drastically Reduced Impacts



Results

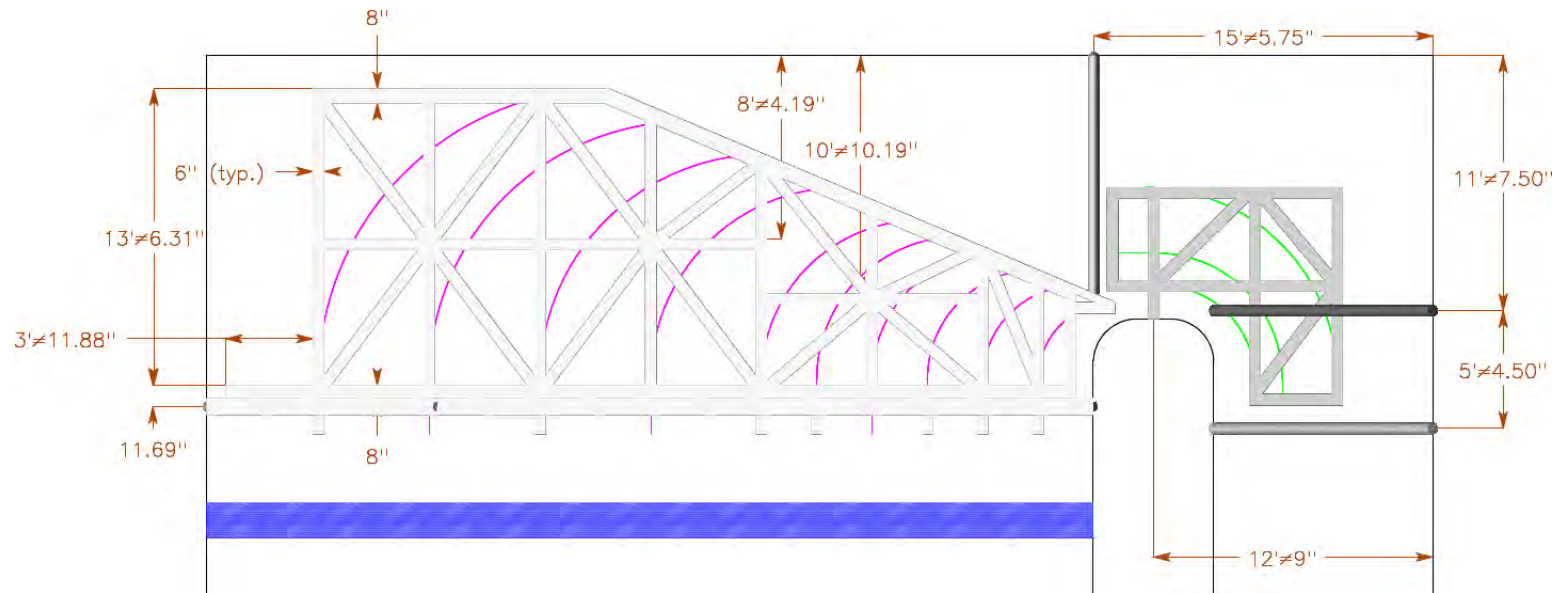
- Initial results, through June 2008, indicate that pressure drop across the screen versus time is staying reasonably stable
- Ian Mylenbush will present recent outage observations

Case 3: Plant Miller Unit 3 SCR Hood Vanes

- Hood vanes designed by original flow modeler
- Severe ash buildup found on the vanes
- Periodically, clumps of ash would avalanche down into the SCR
- How to reduce the buildup?

Hood Vane Geometry

- Big, arching vanes



Buildup

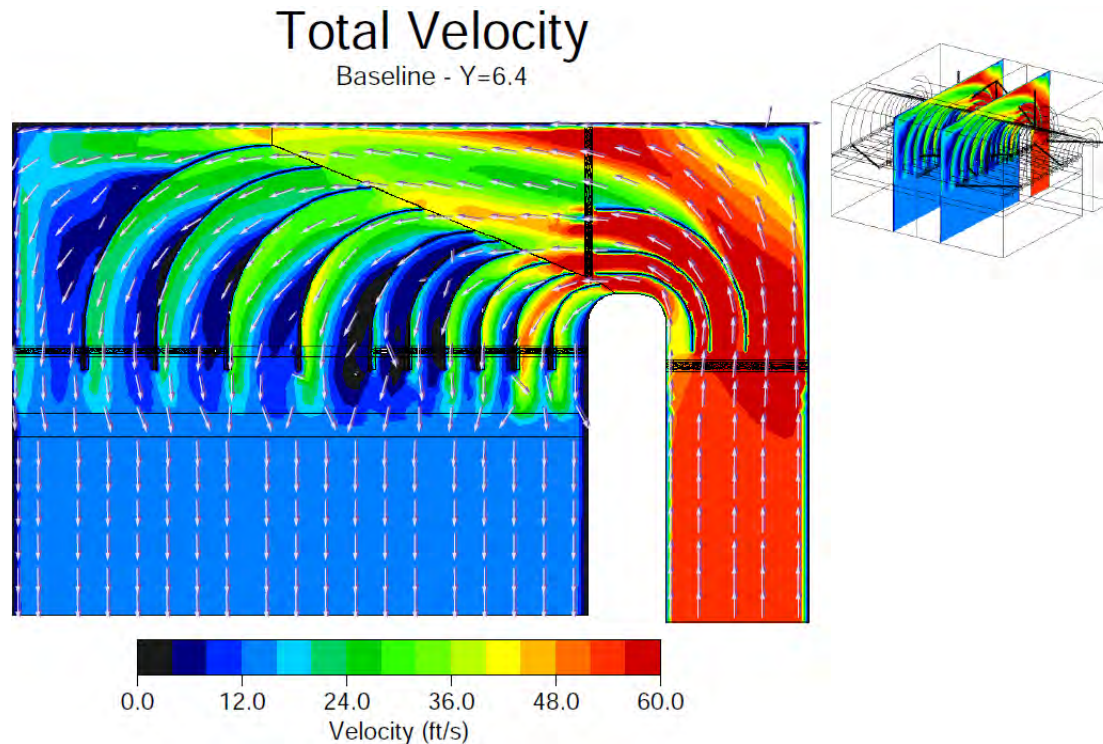


Buildup



Baseline CFD results

- Large areas of low velocity on back sides of vanes
- Ash buildup a concern under 25 fps

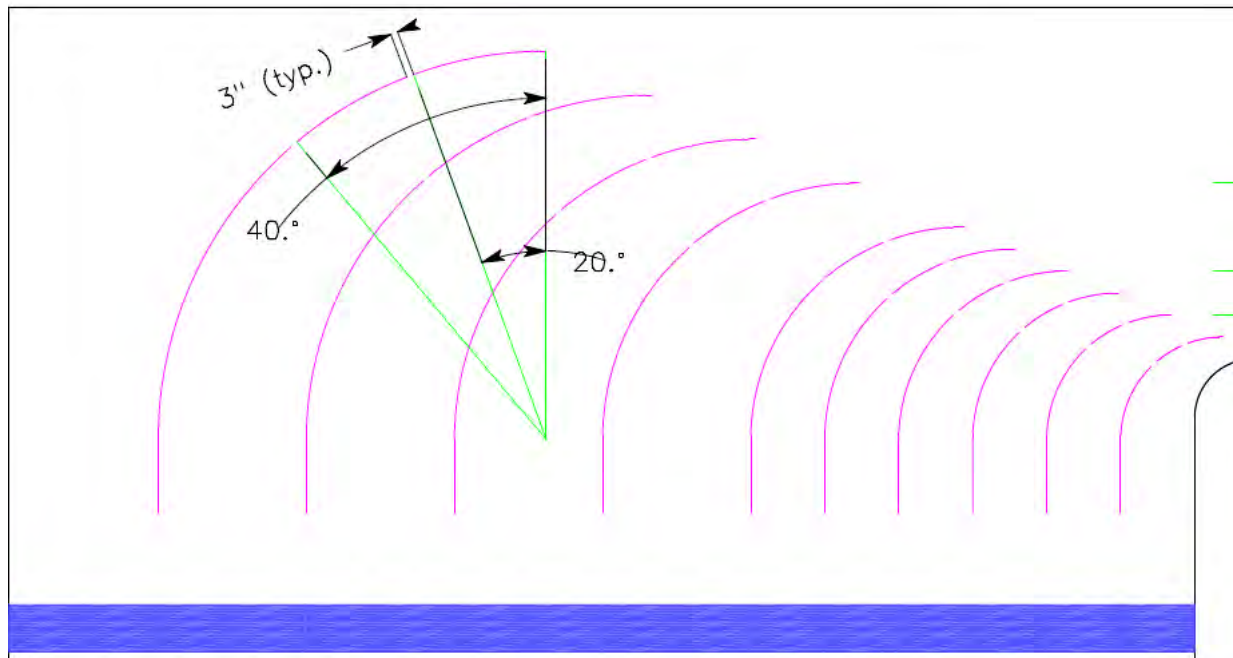


Options?

- Replacing vanes wholesale is deemed too expensive/intrusive
- 3 possible vane modifications stand out
- Critical that modification does 2 things:
 - Reduce ash accumulation
 - Retain flow uniformity at catalyst inlet

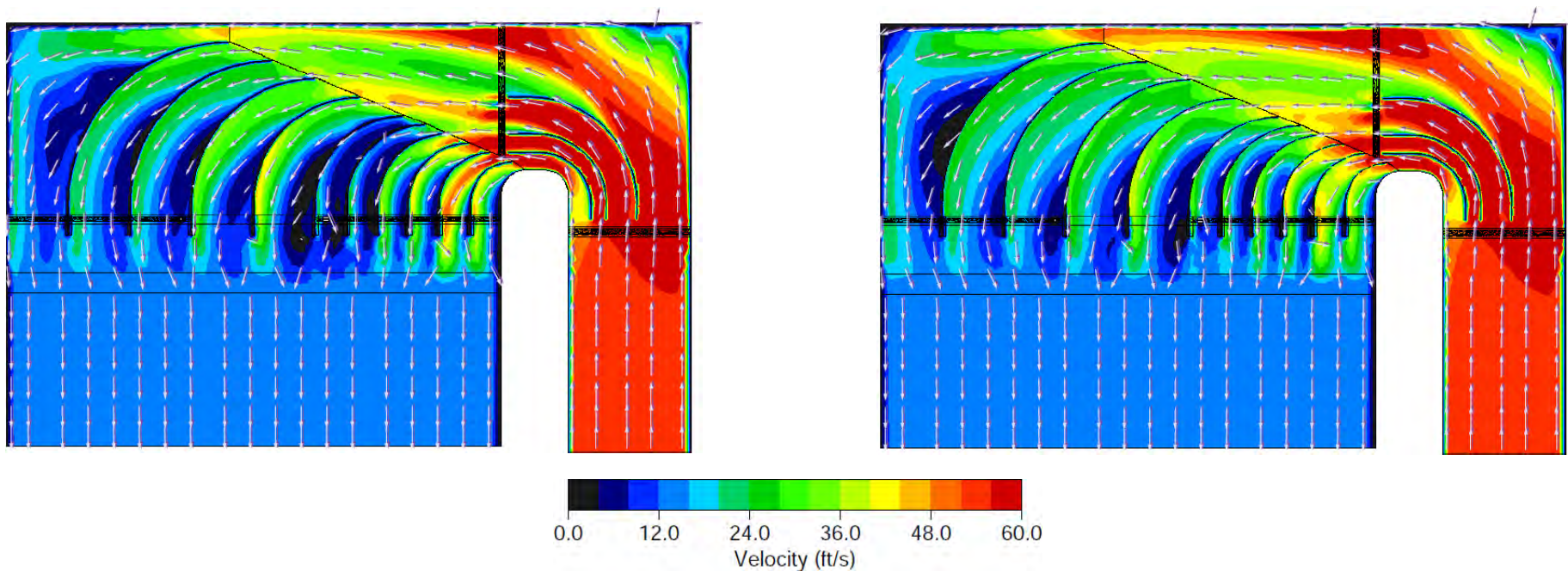
Design 1

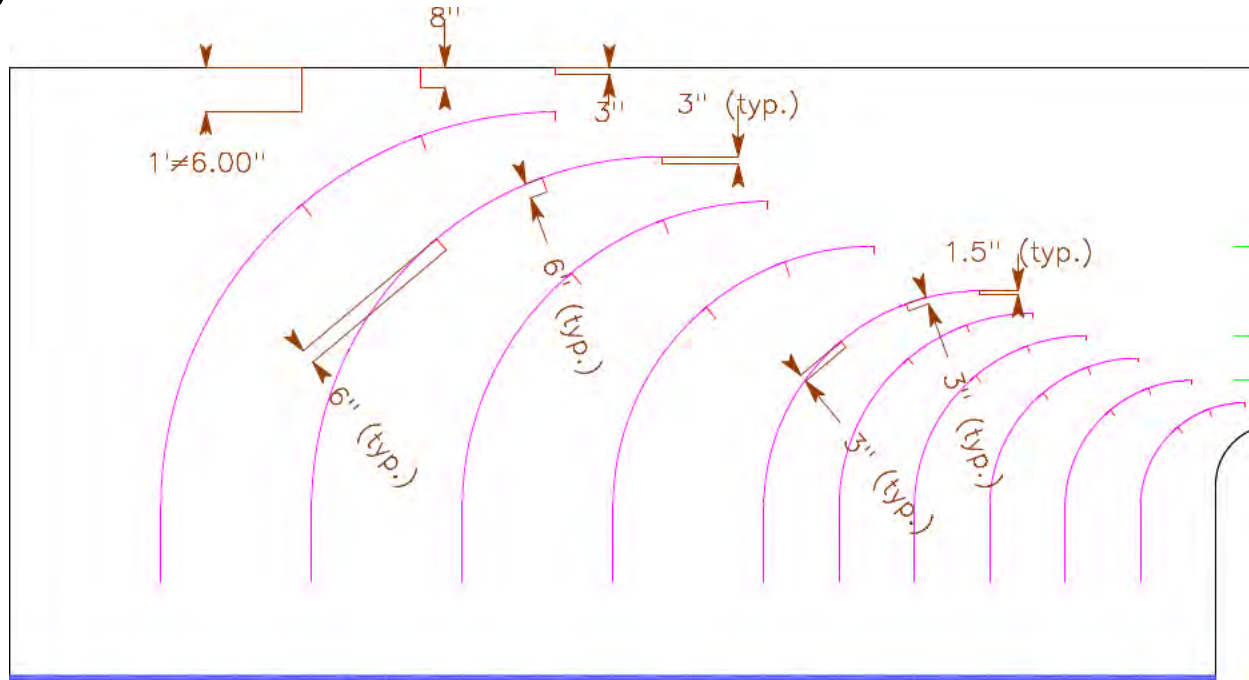
- Long slots cut in vanes
 - 2 slots in each vane along entire width of the vane



Design 1 Results

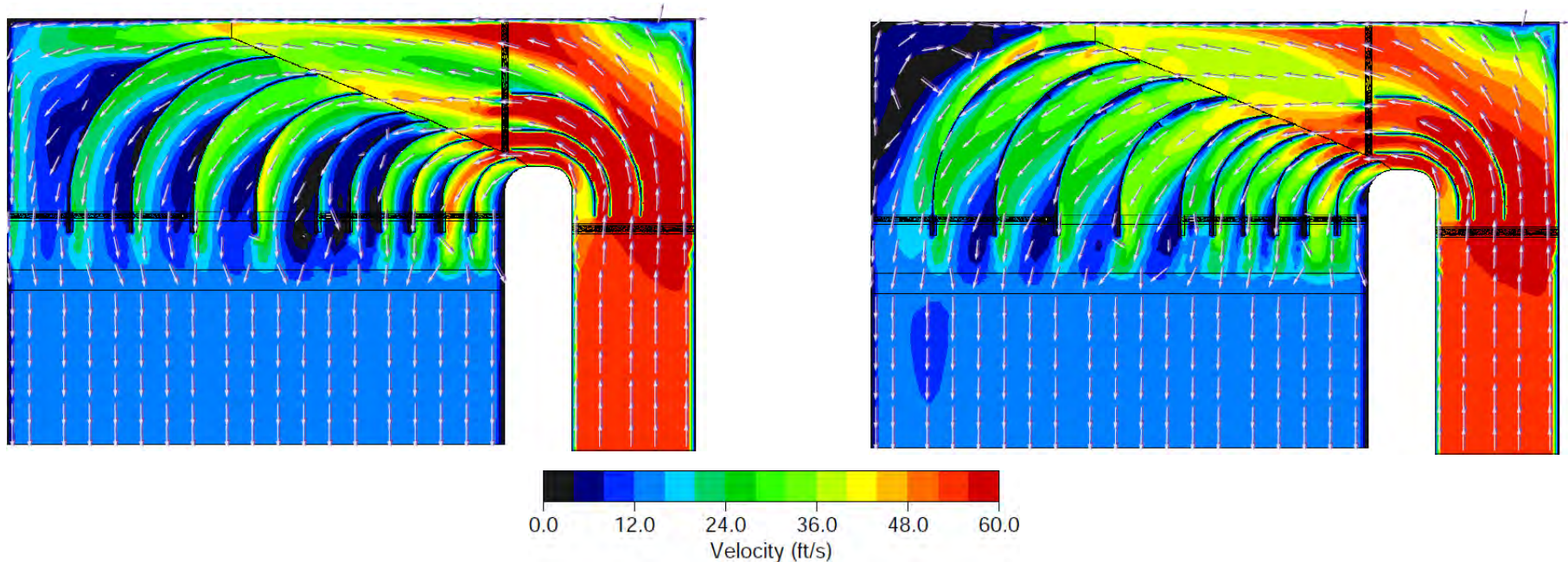
- Reduced low-velocity zones between vanes
- Baseline on left, Design 1 on right





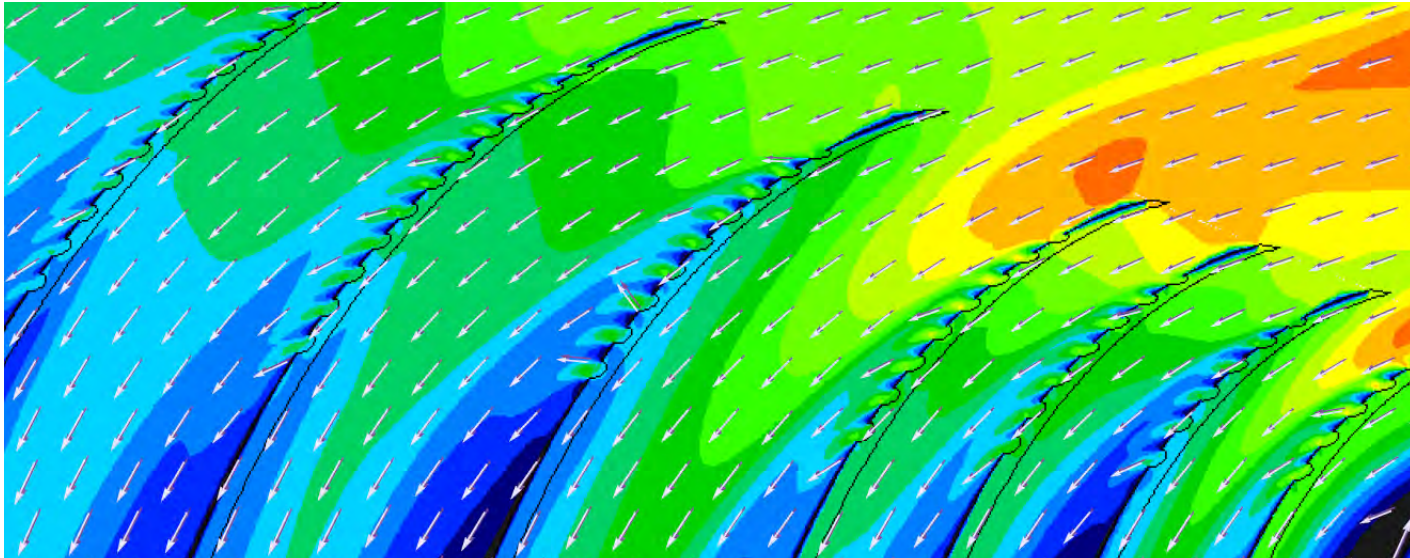
Design 2 Results

- Regions of low velocity are no longer in areas where buildup can occur
- Baseline on left, Design 2 on right



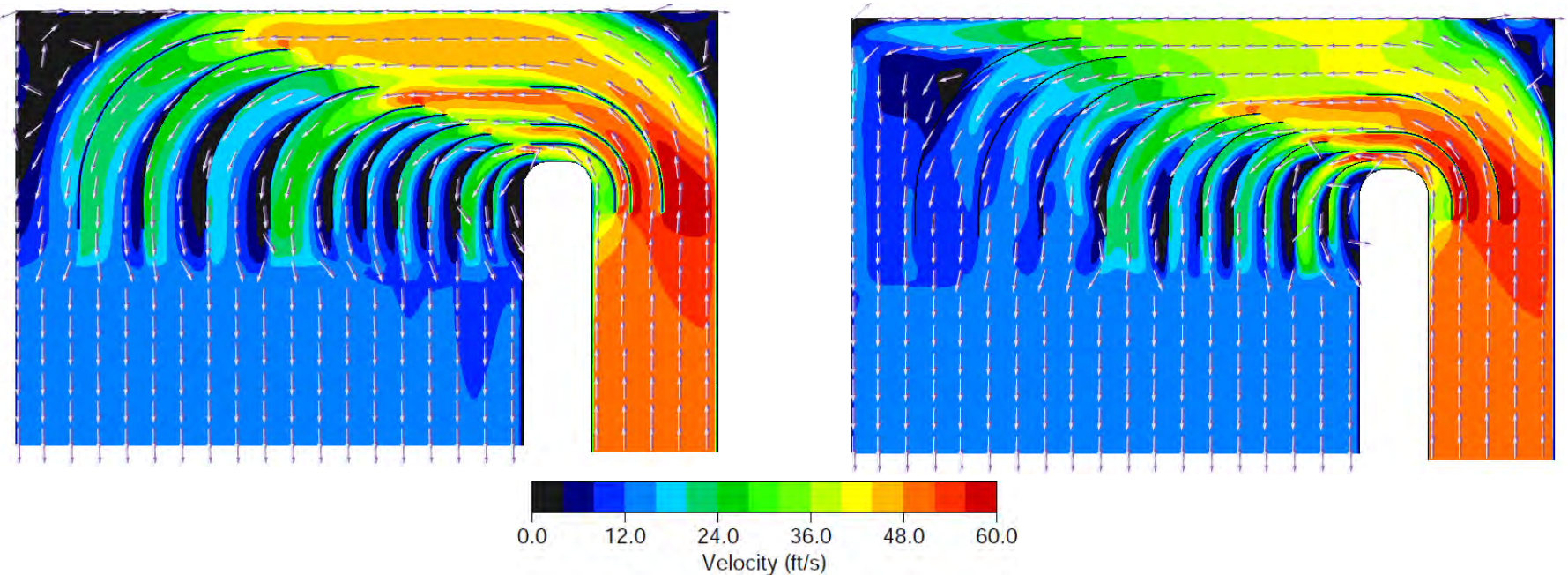
Design 3

- Perforate a portion of each vane
- Very challenging to model – hole details must be included
 - 3d “slice” model employed
 - Inlet conditions differed – new baseline run



Design 3 Results

- Minor global changes, but definite local changes near holes



Which to select?

- All three seem to offer significantly reduced ash accumulation, varying level of difficulty to install
- Plant decides to perform an experiment – install all three in different areas

Questions?

